

ZoomingADC for sensing data acquisition

ADVANCED COMMUNICATIONS & SENSING DATASHEET

DESCRIPTION FEATURES

The SX8725C is a data acquisition system based on Semtech's low power ZoomingADC™ technology. It directly connects most types of miniature sensors with a general purpose microcontroller.

With 1 differential input, it can adapt to multiple sensor systems. Its digital outputs are used to bias or reset the sensing elements.

- Up to 16-bit differential data acquisition
- Programmable gain: (1/12 to 1000)
- Sensor offset compensation up to 15 times full scale of input signal
- \blacksquare 1 differential or 2 single-ended signal inputs
- Programmable Resolution versus Speed versus Supply current
- Digital outputs to bias Sensors
- Internal or external voltage reference
- \blacksquare Internal time base

- Available in tape and reel only

- Low-power (250 uA for $16b \omega$ 250 S/s)
- Fast I2C interface with external address option, no clock stretching required

APPLICATIONS ORDERING INFORMATION

- WEEE/RoHS compliant, Pb-Free and Halogen Free.

 \blacksquare Industrial chemical sensing **Barometer**

Compass

FUNCTIONAL BLOC DIAGRAM

 \blacksquare Industrial pressure sensing **Industrial temperature sensing**

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ELECTRICAL SPECIFICATIONS

1 Absolute Maximum Ratings

Table 1. Absolute Maximum Ratings

Note The Absolute Maximum Ratings, in table below, are stress ratings only. Functional operation of the device at conditions other than those indicated in the Operating Conditions sections of this specification is not implied. Exposure to the absolute maximum ratings, where different to the operating conditions, for an extended period may reduce the reliability or useful lifetime of the product.

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2 Operating Conditions

Unless otherwise specified: VREF,ADC = VBATT, VIN = 0V, Over-sampling frequency $fs = 250$ kHz, PGA3 on with Gain = 1, PGA1&PGA2 off, offsets GDOff2 = GDOff3 = 0. Power operation: normal (IbAmpAdc[1:0] = IbAmpPga[1:0] = '01').

For resolution $n = 12$ bits: $OSR = 32$ and $NELCONV = 4$.

For resolution $n = 16$ bits: $OSR = 256$ and $NELCONV = 2$.

Bandgap chopped at NELCONV rate. If VBATT < 4.2V, Charge Pump is forced on. If VBATT > 4.2V, Charge Pump is forced off.

Table 2. Operating conditions limits

Table 3. Electrical Characteristics

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Table 3. Electrical Characteristics

1. The device can be operated in either active or sleep states. The Sleep state is complete shutdown, but the active state can have a variety of different current consumptions depending on the settings. Some examples are given here: The Sleep state is the default state after power-on-reset. The chip can then be placed into an active state after a valid I2C communication is received.

Table 4. ZoomingADC Specifications

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Table 4. ZoomingADC Specifications

(1) Gain defined as overall PGA gain GDTOT = GD1 x GD2 x GD3. Maximum input voltage is given by: $V_{IN, MAX} = \pm (V_{REF}/2)$ (OSR / OSR+1).

(2) Offset due to tolerance on GDoff2 or GDoff3 setting. For small intrinsic offset, use only ADC and PGA1.

(3) Measured with block connected to inputs through Amux block. Normalized input sampling frequency for input impedance is $f_s = 500$ kHz (fs max, worst case). This figure must be multiplied by 2 for $fs = 250$ kHz, 4 for $fs = 125$ kHz. Input impedance is proportional to 1/fs.

(4) Figure independent from gain and sampling frequency. fS. The effective output noise is reduced by the over-sampling ratio

(5) Resolution is given by n = 2 log2(OSR) + log2(NELCONV). OSR can be set between 8 and 1024, in powers of 2. NELCONV can be set to 1, 2, 4 or 8. (6) If a ramp signal is applied to the input, all digital codes appear in the resulting ADC output data.

(7) Gain error is defined as the amount of deviation between the ideal (theoretical) transfer function and the measured transfer function (with the offset error removed).

(8) Offset error is defined as the output code error for a zero volt input (ideally, output code = 0). For 1 LSB offset, NELCONV must be at least 2.

(9) INL defined as the deviation of the DC transfer curve of each individual code from the best-fit straight line. This specification holds over the full scale.

(10) DNL is defined as the difference (in LSB) between the ideal (1 LSB) and measured code transitions for successive codes.

(11) Values for Gain $= 1$. PSRR is defined as the amount of change in the ADC output value as the power supply voltage changes.

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- (12) Conversion time is given by: $T_{CONV} = (N_{ELCOW} (OSR + 1) + 1) / fs$. OSR can be set between 8 and 1024, in powers of 2. NELCONV can be set to 1, 2, 4 or 8.
- (13) PGAs are reset after each writing operation to registers **RegACCfg1-5**, corresponding to change of configuration or input switching. The ADC should be started only some delay after a change of PGA configuration through these registers. Delay between change of configuration of PGA or input channel switching and ADC start should be equivalent to OSR (between 8 and 1024) number of cycles. This is done by writing bit Start several cycles after PGA settings modification or channel switching. This delay does not apply to conversions made without the PGAs.

New Designs

- (14) Nominal (maximum) bias currents in PGAs and ADC, i.e. $lbbmpPqa[1:0] =$ '11' and $lbbmpAdc[1:0] =$ '11'.
- (15) Bias currents in PGAs and ADC set to 3/4 of nominal values, i.e. IbAmpPga[1:0] = '10', IbAmpAdc[1:0] = '10'. Pents in *PGAs* and *ADC* set to 1/4 of nominal values, i.e. *ibAmpPgg11:01* = 01; *ibAmpAdCl1:01* = 01;
rents in *PGAs* and *ADC* set to 1/4 of nominal values, i.e. *ibAmpPgg11:01* = 00; *ibAmpAdCl1:01* = 00;
rents in *PG*
- (16) Bias currents in PGAs and ADC set to 1/2 of nominal values, i.e. $16AmpPqq[1:0] = 01$ ', $16AmpAdc[1:0] = 01$ '.
- (17) Bias currents in PGAs and ADC set to 1/4 of nominal values, i.e. $16AmpPqq1:0]=100$, $16AmpAcf1:0]=100$.

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2.1 Timing Characteristics

Table 5. General timings

(1) The READY pulse indicates End of Conversion. This is a Positive pulse of duration equal to one cycle of the ADC sampling rate in "continuous mode".

See also **Figure 17, page 33**.

2.1.1 POR Waveforms

At device power-on or after a software reset

Figure 1. Power-On-Reset waveform

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2.1.2 I2C interface timings

Table 6. Digital interface

(1) All timings specifications are referred to VILmin and VIHmax voltage levels defined for the SCL and SDA pins.

(2) The digital interface is reset if the SCL is low more than tscLTO duration. This is the default mode at startup. The timeout can be disabled by register setting.

(3) A Fast-mode I2C-bus device can be used in a Standard-mode I2C-bus system.

(4) The device internally provides a hold time of at least 300 ns for the SDA signal (referred to the VIHmin of the SCL signal) to bridge the undefined region of the falling edge of SCL.

(5) Cb = total capacitance of one bus line in pF. If mixed with Hs-mode devices, faster fall-times according to Table 6 are allowed.

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2.1.3 I2C timing Waveforms

Figure 2. Definition of timing for F/S-mode on the I2C-bus. **New Designs**

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3 Pin Configuration

1.Date codes and Lot numbers starting with the 'E' character are used for Engineering samples

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5 Pin Description

Note The bottom pin is internally connected to VSS. It should also be connected to VSS on PCB to reduce noise and improve thermal behavior.

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6 General Description

The SX8725C is a complete low-power acquisition path with programmable gain, acquisition speed and resolution.

6.1 Bloc diagram

Figure 3. SX8725C bloc diagram

6.2 VREF

The internally generated VREF is a trimmed bandgap reference with a nominal value of 1.22V that provides a stable voltage reference for the ZoomingADC.

This reference voltage is directly connected to one of the ZoomingADC reference multiplexer inputs.

The bandgap voltage stability is only quaranteed for VBATT voltages of 3V and above. As VBATT drops down to 2.4V, the bandgap voltage could reduce by up to 50mV.

The bandgap has relatively weak output drive so it is recommended that if the bandgap is required as a signal input then $PGA1$ must be enabled with gain = 1.

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6.3 GPIO

The GPIO block is a multipurpose 2 bit input/output port. In addition to digital behavior, D0 and D1 pins can be programmed as analog pins in order to be used as output (reference voltage monitoring) and input for an external reference voltage (For further details see **[Figure 6](#page-15-1)**, **[Figure 7](#page-15-2)**, **[Figure 8](#page-15-3)** and **[Figure 9](#page-15-4)**). Each port terminal can be individually selected as digital input or output.

Figure 4. GPIO bloc diagram

The direction of each bit within the GPIO block (input only or input/output) can be individually set using the bits of the **RegOut** (address 0x40) register. If $D[x]Dir = 1$, both the input and output buffer are active on the corresponding GPIO block pin. If D[x]Dir= 0, the corresponding GPIO block pin is an input only and the output buffer is in high impedance. After power on reset the GPIO block pins are in input/output mode $(D[x]Dir)$ are reset to 1).

The input values of GPIO block are available in **RegIn** (address 0x41) register (read only). Reading is always direct - there is no debounce function in the GPIO block. In case of possible noise on input signals, an external hardware filter has to be realized. The input buffer is also active when the GPIO block is defined as output and the effective value on the pin can be read back.

Data stored in the LSB bits of **RegOut** register are outputted at GPIO block if D[x]Dir= 1. The default values after power on reset is low (0).

The digital pins are able to deliver a driving current up to 8 mA.

When the bits VrefD0Out and VrefD1In in the **RegMode** (address 0x70) register are set to 1 the D0 and D1 pins digital behavior are automatically bypassed in order to either input or output the voltage reference signals.

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6.3.1 Optional Operating Mode: External Vref

D0 and D1 are multi-functional pins with the following functions in different operating modes (see **RegMode** register for control settings):

Figure 8. D1 is Digital Input / Output and D0 Reference Voltage Output

Figure 9. D0 is Reference Voltage Output and D1 is Reference Voltage Input

This allows external monitoring of the internal bandgap reference or the ability to use an external reference input for the ADC, or the option to filter the internal VREF output before feeding back as VREF,ADC input. The internally generated VREF is a trimmed as ADC reference with a nominal value of 1.22V. When using an external VREF,ADC input, it may have any value between 0V and VBATT. Simply substitute the external value for 1.22 V in the ADC conversion calculations.

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6.4 Charge Pump

This block generates a supply voltage able to power the analog switch drive levels on the chip higher than VBATT if necessary.

If VBATT voltage drops below 4.2V then the block should be activated. If VBATT voltage is greater than 4.2V then VBATT may be switched straight through to the VPUMP output. If the charge pump is not activated then VPUMP = VBATT.

If control input bit MultForceOff = 1 in **RegMode** (address 0x70) register then the charge pump is disabled and VBATT is permanently connected to VPUMP output.

If control input bit MultForceOn = 1 in **RegMode** register then the charge pump is permanently enabled. This overrides MultForceOff bit in **RegMode** register.

An external capacitor is required on VPUMP pin. This capacitor should be large enough to ensure that generated voltage is smooth enough to avoid affecting conversion accuracy but not so large that it gives an unacceptable settling time. A recommended value is around 2.2nF. ut bit *MultForceOff* = 1 in **RegMode** (address 0x70) register then the charge pump is disconnected to *VPUMP* output.

whist *MultForceOn* = 1 in **RegMode** register then the charge pump is permanently enable

bit in **RegM**

6.5 RC Oscillator

This block provides the master clock reference for the chip. It produces a clock at 4 MHz which is divided internally in order to generate the clock sources needed by the other blocks.

The oscillator technique is a low power relaxation design and it is designed to vary as little as possible over temperature and supply voltage.

This oscillator is trimmed at manufacture chip test.

The RC oscillator will start up after a chip reset to allow the trimming values to be read and calibration registers and I2C address set to their default fused values. Once this has been done, the oscillator will be shut down and the chip will enter a sleep state while waiting for an I2C communication. Example

Interference for the chip. It produces a clock at 4 MHz weded by the other blocks.

It relaxation design and it is designed to vary as little

Interchip test.

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In

The worst case duration from reset (or POR) to the sleep state is 800us.

6.5.1 Wake-up from sleep

When the device is in sleep state, the RC oscillator will start up after a communication. The start up sequence for the RC oscillator is 450us in worst case.

During this time, the internal blocs using the RC can not be used: no ADC conversion can be started.

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7 ZoomingADC

7.1 Overview

The ZoomingADC is a complete and versatile low-power analog front-end interface typically intended for sensing applications. In the following text the ZoomingADC will be referred as ZADC.

The key features of the ZADC are:

- **Programmable 6 to 16-bit dynamic range over-sampled ADC**
- **Flexible gain programming between 1/12 and 1000**
- **Flexible and large range offset compensation**
- Differential or single-ended input
- 2-channel differential reference inputs
- **Power saving modes**

Figure 10. ZADC General Functional Block Diagram

The total acquisition chain consists of an input multiplexer, 3 programmable gain amplifier stages and an over sampled A/D converter. The reference voltage can be selected on two different channels. Two offset compensation amplifiers allow for a wide offset compensation range. The programmable gain and offset allow the application to zoom in on a small portion of the reference voltage defined input range.

7.1.1 Acquisition Chain

[Figure 10, page 18](#page-17-3) shows the general block diagram of the acquisition chain (AC). A control block (not shown in **[Figure 10](#page-17-3)**) manages all communications with the I2C peripheral. The clocking is derived from the internal 4 MHz Oscillator.

Analog inputs can be selected through an 8 input multiplexer, while reference input is selected between two differential channels. It should however be noted that only 7 acquisition channels (including the VREF) are available when configured as single ended since the input amplifier is always operating in differential mode with both positive and negative input selected through the multiplexer.

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The core of the zooming section is made of three differential programmable amplifiers (PGA). After selection of an input and reference signals VIN and VREF,ADC combination, the input voltage is modulated and amplified through stages 1 to 3. Fine gain programming up to 1'000 V/V is possible. In addition, the last two stages provide programmable offset. Each amplifier can be bypassed if needed.

The output of the cascade of PGA is directly fed to the analog-to-digital converter (ADC), which converts the signal VIN,ADC into digital.

Like most ADCs intended for instrumentation or sensing applications, the ZoomingADC TM is an over-sampled converter ¹. The ADC is a so-called incremental converter; with bipolar operation (the ADC accepts both positive and negative differential input voltages). In first approximation, the ADC output result relative to full-scale (FS) delivers the quantity: **[Not](#page-17-3)ify the dependent of the set of the set of the ADC is a so-called incre[me](#page-32-3)ntal converter; with bipolar operation (the ADC accepts be

Recombing ADCTM is an over-

Bendent Manusch De ADC output result relative to full**

Equation 1

FS $\frac{OUT_{ADC}}{T_{ADC}} \cong$

 $2V_{\rm *RFF*}/2$, *REF*

 $ADC \sim$ ^VIN,ADC *V V*

in two's complement (see **Equation 18** and **Equation 19, page 33** for details). The output code OUTADC is -FS / 2 to + FS / 2 for VIN,ADC = -VREF,ADC / 2 to + VREF,ADC / 2 respectively. As will be shown, VIN,ADC is related to input voltage VIN by the relationship: Equation 1
 Equation 19, page 33 for details). The output

EF,ADC / 2 respectively. As will be shown, VIN,ADC is re

W_{N,ADC} = $GD_{TOT} \cdot V_{IN}$ - $GD_{Off_{TOT}} \cdot S \cdot V_{REF}$ [V]
 Equation 2

PFFTOT is the total magnitude of *PGA*

Equation 2

where GDTOT is the total PGA gain, GDOFFTOT is the total magnitude of PGA offset and S is the sign of the offset (see **[Table 9, page 21](#page-20-1)**).

7.1.2 Programmable Gain Amplifiers

As seen in **Figure 10, page 18**, the zooming function is implemented with three programmable gain amplifiers (PGA). These are:

- $PGA1$: coarse gain tuning
- **PGA2: medium gain and offset tuning**
- PGA3: fine gain and offset tuning. Should be set ON for high linearity data acquisition

All gain and offset settings are realized with ratios of capacitors. The user has control over each PGA activation and gain, as well as the offset of stages 2 and 3. These functions are examined hereafter.

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^{1.} Over-sampled converters are operated with a sampling frequency fs much higher than the input signal's Nyquist rate (typically fs is 20-1'000 times the input signal bandwidth). The sampling frequency to throughput ratio is large (typically 10-500). These converters include digital decimation filtering. They are mainly used for high resolution, and/or low-to-medium speed applications.

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7.1.3 PGA & ADC Enabling

Depending on the application objectives, the user may enable or bypass each PGA stage. This is done according to the word Enable and the coding given in **[Table 7](#page-19-4)**. To reduce power dissipation, the ADC can also be inactivated while idle.

Table 7. ADC and PGA Enabling

7.2 ZoomingADC Registers

The system has a bank of eight 8-bit registers: six registers are used to configure the acquisition chain (**RegAcCfg0** to **RegAcCfg5**), and two registers are used to store the output code of the analog-to-digital conversion (**RegAcOutMsb** & **Lsb**).

Table 8. Periferal Registers to Configure the Acquisition Chain (AC) and to Store the Analog-to-Digital Conversion (ADC) Result

 $(r = read; w = write; rw = read & write)$

(1) **Out**: (r) digital output code of the analog-to-digital converter. (MSB = Out[15])

(2) **Start**: (w) setting this bit triggers a single conversion (after the current one is finished). This bit always reads back 0.

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- (3) **SetNelconv**: (rw) sets the number of elementary conversions to 2(SetNelconv[1:0]). To compensate for offsets, the input signal is chopped between elementary conversions (1,2,4,8).
- (4) **SetOsr**: (rw) sets the over-sampling rate (OSR) of an elementary conversion to $2^{(3+SetOsr[2:0J)}$. OSR = 8, 16, 32, ..., 512, 1024.
- (5) **Continuous**: (rw) setting this bit starts a conversion. When this bis is 1, A new conversion will automatically begin directly when the previous one is finished.
- (6) Reserved
- (7) **IbAmpAdc**: (rw) sets the bias current in the ADC to 0.25 x (1+ IbAmpAdc[1:0]) of the normal operation current (25, 50, 75 or 100% of nominal current). To be used for low-power, low-speed operation.
- (8) **IbAmpPga**: (rw) sets the bias current in the PGAs to 0.25 x (1+IbAmpPga[1:0]) of the normal operation current (25, 50, 75 or 100% of nominal current). To be used for low-power, low-speed operation.
- (9) **Enable**: (rw) enables the ADC modulator (bit 0) and the different stages of the PGAs (PGAi by bit i=1,2,3). PGA stages that are disabled are bypassed.
- (10) **SetFs**: (rw) These bits set the over sampling frequency of the acquisition chain. Expressed as a fraction of the oscillator frequency, the sampling frequency is given as: 11 ' 500 kHz, 10 ' 250 kHz, 01 ' 125 kHz, 00 ' 62.5 kHz.
- (11) **Pga1Gain**: (rw) sets the gain of the first stage: 0 ' 1, 1 ' 10.
- (12) **Pga2Gain**: (rw) sets the gain of the second stage: 00 ' 1, 01 ' 2, 10 ' 5, 11 ' 10.
- (13) **Pga3Gain**: (rw) sets the gain of the third stage to Pga3Gain[6:0] 1/12.
- (14) **Pga2Offset**: (rw) sets the offset of the second stage between -1 and +1, with increments of 0.2. The MSB gives the sign (0 positive, 1 negative); amplitude is coded with the bits Pga2Offset[5:0].
- (15) **Pga3Offset**: (rw) sets the offset of the third stage between -5.25 and +5.25, with increments of 1/12. The MSB gives the sign (0 positive, 1 negative); amplitude is coded with the bits Pga3Offset[5:0].
- (16) **Busy**: (r) set to 1 if a conversion is running.
- (17) **Def**: (w) sets all values to their defaults (PGA disabled, max speed, nominal modulator bias current, 2 elementary conversions, over-sampling rate of 32) and starts a new conversion without waiting the end of the preceding one.
- (18) **Amux**(4:0): (rw) Amux[4] sets the mode (0 ' differential inputs, 1 ' single ended inputs with A0= common reference) Amux[3] sets the sign (0 ' straight, 1' cross) Amux[2:0] sets the channel.
- (19) **Vmux**: (rw) sets the differential reference channel (0 ' *VBATT_, 1 ' VREF*).

7.3 Input Multiplexers (AMUX and VMUX)

 ϕ^*

The ZoomingADC has analog inputs AC0 to AC3 and reference inputs. Let us first define the differential input voltage VIN and reference voltage VREF,ADC respectively as: If low-power, [ow-speed operation.

The for *Recognent* of the profile of the and the control of the normal operation current (25, 5

For low-power, low-speed operation.

ADC modulator (bit 0) and the different stages of *Pga2Offset[5:0].*

hird stage between -5.25 and +5.25, with increments of 1/12.1

bits *Pga3Offset[5:0]*.

ng.

(*PGA* disabled, max speed, nominal modulator bias current, 2

(*PGA* disabled, max speed, nominal modulator

$$
V_{IN} = V_{INP} - V_{INN} \qquad [V]
$$

Equation 3

$$
V_{REF} = V_{REFP} - V_{REFN} \qquad [V]
$$

Equation 4

As shown in **[Table 9](#page-20-1)**, the inputs can be configured in two ways: either as 4 differential channels (VIN1= AC1 - AC0, VIN2 = AC3 - AC2), or AC0 can be used as a common reference, providing 7 signal paths all referred to AC0. The control word for the analog input selection is Amux. Notice that the Amux bit 4 controls the sign of the input voltage.

Table 9. Analog Input Selection

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Table 9. Analog Input Selection

Similarly, the reference voltage is chosen among two differential channels (VREF = VBATT-VSS, VREF = VBG-VSS or VREF = VREF,IN-VSS) as shown in **Table 10**. The selection bit is Vmux. The reference inputs VREFP and VREFN (common-mode) can be up to the power supply range.

Table 10. Analog reference Input Selection

1. External voltage reference on D1 GPIO pin. See **section 6.3 on page 15** about GPIO and "RegMode[0x70]" on page 46.

7.4 First Stage Programmable Gain Amplifier (PGA1)

The first stage can have a buffer function (unity gain) or provide a gain of 10 (see **Table 11**). The voltage VD1 at the output of PGA1 is:

$$
V_{D1} = GD_1 \cdot V_{IN} \qquad [V]
$$

Equation 5

where GD1 is the gain of PGA1 (in V/V) controlled with the Pga1Gain bit.

Table 11. PGA1 gain settings

Pga1Gain bit (RegACCfg3[7])	PGA1 gain [V/V] GD_1 [V/V]
	10

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7.5 Second Stage Programmable Gain Amplifier (PGA2)

The second PGA has a finer gain and offset tuning capability, as shown in **[Table 12](#page-22-4)**. The VD2 voltage at the output of PGA2 is given by:

 $V_{D2} = GD_2 \cdot V_{D1} - GD\text{off}_2 \cdot S \cdot V_{REF}$ [V]

Equation 6

Table 12. PGA2 gain and offset settings

where GD2 and GDOFF2 are respectively the gain and offset of PGA2 (in V/V). These are controlled with the words Pga2Gain[1:0] and Pga2Offset[3:0].

Pga2Offset bitfield (RegACCfg2[3:0]) PGA2 offset GDOFF2 [V/V] 00 1 1 0000 0 01 2 0001 +0.2 10 10 5 0010 +0.4 11 10 10 0011 +0.6 $0100 +0.8$ $0101 +1$ 1000 0 1001 -0.2 1010 -0.4 1011 -0.6 1100 -0.8 1101 -1.0 Equation 6

McGDoFF2 are respectively the gain and offset of PGA2 (in V/V). These are controlled with

(in Pga2Gifset[3:0].

Table 12. PGA2 gain and offset settings

Pga2Gifset[3:30].

Table 12. PGA2 gain (V/V)

Table 12. 1

1

2

5

10

0001

5

0010

+0.2

+0.4

+0.4

0010

+0.6

0100

+0.8

0101

+1

1000

0

011

+1

1000

0

0101

+1

001

-0.6

0101

-

7.6 Third Stage Programmable Gain Amplifier (PGA3)

The finest gain and offset tuning is performed with the third and last PGA stage, according to the coding of **[Table 13](#page-22-5)**.

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Table 13. PGA3 Gain and Offset Settings

The output of PGA3 is also the input of the ADC. Thus, similarly to PGA2, we find that the voltage entering the ADC is given by:

$$
V_{IN, ADC} = GD_3 \cdot V_{D2} - GDoff_3 \cdot S \cdot V_{REF} \quad [V]
$$

Equation 7

where GD3 and GDOFF3 are respectively the gain and offset of PGA3 (in V/V). The control words are Pga3Gain[6:0] and Pga3Offset[6:0]. $N_{N,ADC} = GD_3 \cdot V_{D2} - GDoff_3 \cdot S \cdot V_{REF}$ [V]
 Equation 7
 Noting the gain and offset of PGA3 (in V/V). The control with the pGA stages (no saturation), the condition:
 $|V_{IN}|, |V_{D1}|, |V_{D2}| < \frac{V_{BAT}}{2}$
 Equation 8

To remain within the signal compliance of the PGA stages (no saturation), the condition:

$$
|V_{IN}|, |V_{D1}|, |V_{D2}| < \frac{V_{BAT}}{2}
$$

Equation 8

must be verified. To remain within the signal compliance of the ADC (no saturation), the condition:

$$
\left|V_{\text{IN,ADC}}\right| < \left(\frac{V_{\text{REF}}}{2}\right)\left(\frac{\text{OSR}-1}{\text{OSR}}\right)
$$

Equation 9

must be verified.

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Finally, combining **[Equation 5](#page-21-4)** to **[Equation 7](#page-23-0)** for the three PGA stages, the input voltage VIN,ADC of the ADC is related to VIN by:

$$
V_{IN, ADC} = GD_{TOT} \cdot V_{IN} - GDoff_{TOT} \cdot S \cdot V_{REF} \quad [V]
$$

Equation 10

where the total PGA gain is defined as:

 $GD_{TOT} = GD_3 \cdot GD_2 \cdot GD_1$

Equation 11

and the total PGA offset is:

 $GDoff_{TOT} = GDoff_3 + GD_3 \cdot GDoff_3$

Equation 12

7.6.1 PGA Ranges

[Figure 11](#page-25-0) and **Figure 12** illustrates the limits for the maximal conversion precision according to the common mode voltage (VCOMMON), the ADC over-sampling frequency (fs) and PGA gains. The best linearity performances can be Equation 10

Equation 11

FGA offset is:
 $GD_{TOT} = GD_3 \cdot GD_2 \cdot GD_1$

Equation 11

PGA offset is:
 $GDoff_{TOT} = GD_0ff_2 + GD_1 \cdot GD_0ff_2$

Equation 12
 Ranges
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 Ranges
 Ranges $GDef_{TOT} = GDef_{3} + GD_{3} \cdot GD_{0}f_{2}$
 Equation 12
 Equation 12
 Elimits for the maximal conversion precision according frequency (fs) and PGA gains. The best linearify

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obtained only below these limits, as depicted in **[Figure 11](#page-25-0)** if the supply voltage (VBATT) is below 4.2V and as depicted in **[Figure 12](#page-26-0)** if the supply voltage (VBATT) is above 4.2V.

Figure 11. Common mode input range on PGA for VBATT below 4.2V

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Figure 12. Common mode input range on PGA for VBATT above 4.2V

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7.7 Analog-to-Digital Converter (ADC)

The main performance characteristics of the ADC (resolution, conversion time, etc.) are determined by three programmable parameters. The setting of these parameters and the resulting performances are described later.

- f_s : Over-sampling frequency
- OSR: Over-Sampling Ratio
- NELCONV: Number of Elementary Conversions

7.7.1 Conversion Sequence

A conversion is started each time the bit Start or the Def bit is set. As depicted in **Figure 14**, a complete analog-todigital conversion sequence is made of a set of NELCONV elementary incremental conversions and a final quantization step. Each elementary conversion is made of (OSR+1) over-sampling periods $Ts=1/fs$, i.e.:

$T_{ELCONV} = (OSR+1)/f_s$

Equation 13

The result is the mean of the elementary conversion results. An important feature is that the elementary conversions are alternatively performed with the offset of the internal amplifiers contributing in one direction and the other to the output code. Thus, converter internal offset is eliminated if at least two elementary sequences are performed (i.e. if NELCONV >= 2). A few additional clock cycles are also required to initiate and end the conversion properly.

internal offset voltage and 1/fs noise.

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7.7.2 Over-Sampling Frequency (fs)

The word SetFs[1:0] (see **[Table 14](#page-28-3)**) is used to select the over-sampling frequency fs. The over-sampling frequency is derived from the 4MHz oscillator clock.

Table 14. Sampling frequency settings

7.7.3 Over-Sampling Ratio (OSR)

The over-sampling ratio (OSR) defines the number of integration cycles per elementary conversion. Its value is set with the word SetOsr[2:0] in power of 2 steps (see **Table 15**) given by:

$OSR = 2^{3+SetOsr[2:0]}$

Equation 14

Table 15. Over-sampling ratio settings

7.7.4 Number of Elementary Conversions (Nelconv)

As mentioned previously, the whole conversion sequence is made of a set of NELCONV elementary incremental conversions. This number is set with the word SetNelconv[1:0] in power of 2 steps (see **[Table 16](#page-29-1)**) given by:

$$
N_{\text{ELCONV}} = 2^{\text{SetNelconv}[1:0]} \quad [-]
$$

Equation 15

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Table 16. Number of elementary conversion

As already mentioned, NELCONV must be equal or greater than 2 to reduce internal amplifier offsets.

7.7.5 Resolution

The theoretical resolution of the ADC, without considering thermal noise, is given by:

 $n = 2 \cdot \log_2(OSR) + \log_2(N_{ELCON})$ [bit

Equation 16

Figure 15. Resolution vs. SetOsr[2:0] and SetNelconv[2:0]

Using look-up **[Table 17](#page-30-1)** or the graph plotted in **[Figure 15](#page-29-2)**, resolution can be set between 6 and 16 bits. Notice that, because of 16-bit register use for the ADC output, **practical resolution is limited to 16 bits**, i.e. n = 16. Even if the

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resolution is truncated to 16 bit by the output register size, it may make sense to set OSR and N_{ELCONV} to higher values in order to reduce the influence of the thermal noise in the PGA .

Table 17. Resolution¹ vs. SetOsr and SetNelconv settings

1. In shaded area, the resolution is truncated to 16 bits due to output register size **RegA-COut[15:0]**

7.7.6 Conversion Time & Throughput

As explained in **Figure 15**, conversion time is given by:

```
T_{conv} = (N_{ELCONV} \cdot (OSR+1)+1)/f_s [s]
```
Equation 17

and throughput is then simply 1/Tconv. For example, consider an over-sampling ratio of 256, 2 elementary conversions, and a sampling frequency of 500 kHz (SetOsr = "101", SetNelconv = "01" and SetFs = "00"). In this case, using **[Table 18](#page-30-2)**, the conversion time is 515 sampling periods, or 1.03ms. This corresponds to a throughput of 971Hz in continuous-time mode. The plot of **Figure 16** illustrates the classic trade-off between resolution and conversion time.

Table 18. Normalized conversion time (Tconv x fs) vs. SetOsr and SetNelconv settings¹

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Table 18. Normalized conversion time (Tconv x fs) vs. SetOsr and SetNelconv settings¹

1. Normalized to sampling period 1/fs

Figure 16. Resolution vs. normalized¹ conversion time for different SetNelconv[1:0]

1. Normalized Conversion Time - Tconv/fs

7.7.7 Continuous-Time vs. On-Request Conversion

The ADC can be operated in two distinct modes: "continuous-time" and "on-request" modes (selected using the bit Continuous).

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In "continuous-time" mode, the input signal is repeatedly converted into digital. After a conversion is finished, a new one is automatically initiated. The new value is then written in the result register, and the corresponding internal trigger pulse is generated. This operation is sketched in **[Figure 17](#page-32-4)**. The conversion time in this case is defined as TCONV.

Figure 17. ADC "Continuous-Time" Operation

In the "on-request" mode, the internal behavior of the converter is the same as in the "continuous-time" mode, but the conversion is initiated on user request (with the Start bit). As shown in **Figure 18**, the conversion time is also TCONV.

Figure 18. ADC "On-Request" Operation

7.7.8 Output Code Format

The ADC output code is a 16-bit word in two's complement format (see **Table 19**). For input voltages outside the range, the output code is saturated to the closest full-scale value (i.e. 0x7FFF or 0x8000). For resolutions smaller than 16 bits, the non-significant bits are forced to the values shown in **Table 20**. The output code, expressed in LSBs, corresponds to:

$$
OUT_{ADC} = 2^{16} \cdot \frac{V_{IN,ADC}}{V_{REF}} \cdot \frac{OSR + 1}{OSR}
$$

Equation 18

Recalling **[Equation 10, page 25](#page-24-1)**, this can be rewritten as:

$$
OUT_{ADC} = 2^{16} \cdot \frac{V_{IN}}{V_{REF}} \cdot \left(GD_{TOT} - GDoff_{TOT} \cdot S \cdot \frac{V_{REF}}{V_{IN}}\right) \cdot \frac{OSR + 1}{OSR} \quad [LSB]
$$

Equation 19

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where, from **[Equation 11](#page-24-2)** and **[Equation 12](#page-24-3)**, the total PGA gain and offset are respectively:

 $GD_{TOT} = GD_3 \cdot GD_2 \cdot GD_1$

Equation 20

and:

$$
G\text{Doff}_{\text{TOT}} = G\text{Doff}_3 + G\text{D}_3 \cdot G\text{Doff}_2
$$

Equation 21

Table 19. Basic ADC Relationships (example for: VREF = 5V, OSR = 512, n = 16bits)

1. (n<16) (RegACOutMsb[7:0] & RegACOutLsb[7:0])

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The equivalent LSB size at the input of the PGA chain is:

$$
LSB = \frac{1}{2^n} \cdot \frac{V_{REF}}{GD_{TOT}} \cdot \frac{OSR}{OSR+1} \quad [V/V]
$$

Equation 22

Notice that the input voltage $V_{IN, ADC}$ of the ADC must satisfy the condition:

$$
\left|V_{\text{IN,ADC}}\right| \leq \frac{1}{2} \cdot \left(V_{\text{REFP}} - V_{\text{REFN}}\right) \cdot \frac{OSR}{OSR + 1}
$$

Equation 23

to remain within the ADC input range.

7.7.9 Power Saving Modes

During low-speed operation, the bias current in the PGAs and ADC can be programmed to save power using the control words IbAmpPga[1:0] and IbAmpAdc[1:0] (see **Table 21**). If the system is idle, the PGAs and ADC can even be disabled, thus, reducing power consumption to its minimum. This can considerably improve battery lifetime.

Table 21. ADC & PGA power saving modes and maximum sampling frequency

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8 Application hints

8.1 Power Reduction

The ZoomingADC is particularly well suited for low-power applications. When very low power consumption is of primary concern, such as in battery operated systems, several parameters can be used to reduce power consumption as follows:

- Operate the acquisition chain with a reduced supply voltage VBATT.
- Disable the PGAs which are not used during analog-to-digital conversion with *Enable*[3:0].
- Disable all PGAs and the ADC when the system is idle and no conversion is performed.
- **Use lower bias currents in the PGAs and the ADC using the control words IbAmpPga[1:0] and IbAmpAdc[1:0].**
- Reduce sampling frequency.

Finally, remember that power reduction is typically traded off with reduced linearity, larger noise and slower maximum sampling speed. the acquisition chain with a reduced supply voltage *VBAT*.

Ne *PGAs* which are not used during nanlog-to-digital conversion with *Enable*[3:0].

Il *PGAs* and the *ADC* when the system is ide and no conversion is perform

New Designs

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8.2 Gain Configuration Flow

The diagram below shows the flow to set the gain of your configuration:

Figure 19. Gain configuration flowchart

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9 I2C Interface

The I2C interface gives access to the chip registers. It complies with the I2C protocol specifications, restricted to the slave side of the communication.

The device uses a Generic Fast-Mode (400 KHz) I2C Slave Interface in accordance with the I2C bus standard. Its characteristics can be summarized as follows:

9.1 General Features

- Slave only operation
- Fast mode operation (up to 400 kHz)
- Combined read and write mode support
- General call reset support
- 7-bits default slave address 0x48. Can be changed by fuse and by pinout (D0 and D1).

The interface handles I2C communication at the transaction level. A read transaction is an external request to get the content of system memory location and a write transaction is an external request to write the content of a system memory location. **Note that the metallal series are above that the series of the serve that the server the server of the dial server detail and the that state support (and the state support and the transaction level. A read transaction is**

The default I2C slave address is 0x48, 1001000 in binary. This is the standard part I2C slave address. Other addresses between 1000000 and 1001111 are available. 001000 in binary. This is the standard part I2C slave
ailable.
ns
fuse-programmed bits + 2 LSBs given by 2 GPIO in
) can be changed in production by fuse. Other value
ales for more information. Otherwise, default value
c

9.2 Other Slave Address Options

Slave address might be diffenciated (2 fuse-programmed bits + 2 LSBs given by 2 GPIO inputs):

- Address bit 3 and bit 2 (100**XX**xx) can be changed in production by fuse. Other values are available by special request. Please contact Semtech Sales for more information. Otherwise, default value is "00".
- The last significant bits (100xx**XX**) can be defined by the GPIO pin D0 and D1. This mode is not set by default at startup, it must be activated in a register with a command. Default value is "00".

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9.2.1 Address Set Externally

Figure 20. Example of I2C address set by external resistors

The GPIO are set as ouput low at startup, so a resistor should be connected to the pad to avoid shortcut at startup. After startup, the master I2C can send a command (0x96 in RegExtAdd[0x43]) at the default I2C address to change I2C mode and set D0 and D1 as input address bits.

If several SX87xx devices are connected on the same bus, the master MCU must send the command to each device simultaneousely using the default address. All SX87xx devices will receive the command at the same time. The master MCU must ensure that the command has been received by asking each slave device at their new address.

9.3 I2C General Call Reset

The device respond to the I2C general call address (0000000) if the eighth bit is '0'. The devices acknowledge the general call address and respond to commands in the second byte. If the second byte is 00000110 (06h), the device reset the internal registers and enter power-down mode. 20. Example of l2C address set by external resistors
up, so a resistor should be connected to the pad to a
a command (0x96 in RegExtAdd[0x43]) at the defaulties
so bits.
d on the same bus, the master MCU must send the
ress

Figure 21. I2C General Call reset frame

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9.4 I2C Register Access

9.4.1 Writing a Register

9.4.2 Reading in a Register

Figure 23. I2C timing diagram for reading from a register

9.4.3 Writing in Several Consecutive Registers

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9.4.4 Reading from Several Consecutive Registers

Figure 25. I2C timing diagram for multiple reading from a register

New Designs

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10 Register Memory Map and Description

10.1 Register Map

[Table 22](#page-41-3) below describes the register/memory map that can be accessed through the I2C interface. It indicates the register name, register address and the register contents.

Table 22. Register Map

10.2 Registers Descriptions

The register descriptions are presented here in ascending order of Register Address. Some registers carry several individual data fields of various sizes; from single-bit values (e.g. flags), upwards. Some data fields are spread across multiple registers. After power on reset the registers will have the values indicated in the tables "Reset" column. Please write the "Reserved" bits with their reset values.

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10.2.1 RC Register

Table 23. RegRCen[0x30]

10.2.2 GPIO Registers

Table 24. RegOut[0x40]

Table 25. RegIn[0x41]

Table 26. RegTimout[0x42]

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Table 27. RegExtAdd[0x43]

10.2.3 ZADC Registers

Table 28. RegACOutLsb[0x50]

Table 29. RegACOutMsb[0x51]

Table 30. RegACCfg0[0x52]

Table 31. RegACCfg1[0x53]

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Table 32. RegACCfg2[0x54]

Table 33. RegACCfg3[0x55]

Table 34. RegACCfg4[0x56]

Table 35. RegACCfg5[0x57]

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10.2.4 Mode Registers

Table 36. RegMode[0x70]

(1) The chop control is to allow chopping of the internal bandgap reference. This may be useful to help eliminate bandgap related internal offset voltage and 1/f noise. The bandgap chop state may be forced High or Low, or may be set to toggle during conversion at either the same rate or half the rate of the Elementary Conversion. (See Conversion Sequence in the ZoomingADC description). Final bandgap reference. This may be useful to help
ap chop state may be forced High or Low, or may be set to tog
tary Conversion. (See Conversion Sequence in the ZoomingAD
d On when *VBATT* supply is below 4.2V or Off whe

(2) The internal charge pump may be forced On when VBATT supply is below 4.2V or Off when VBATT supply is above 4.2V. Enabling the charge pump increase the current consumption. If the ADC is not being run at full rate or full accuracy then it may operate sufficiently well when VBATT is less than 4.2V and internal charge pump forced Off.

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11 Typical Performances

Note The graphs and tables provided following this note are statistical summary based on limited number of samples and are provided for informational purposes only. The performance characteristics listed herein are not tested or guaranteed. In some graphs or tables, the data presented may be outside the specified operating range and therefore outside the warranted range.

11.1 Input impedance

The PGAs of the ZoomingADC are a switched capacitor based blocks (see Switched Capacitor Principle section). This means that it does not use resistors to fix gains, but capacitors and switches. This has important implications on the nature of the input impedance of the block.

Using switched capacitors is the reason why, while a conversion is done, the input impedance on the selected channel of the PGAs is inversely proportional to the sampling frequency fs and to stage gain as given in **[Equation 24](#page-46-3)**.

$$
Z_{in} \ge \frac{1}{f_s \cdot (Cg \cdot gain + Cp)} \quad [\Omega]
$$

Equation 24

The input impedance observed is the input impedance of the first PGA stage that is enabled or the input impedance of the ADC if all three stages are disabled.

Cq multiplied by gain is the equivalent gain capacitor and C_p is the parasitic capacitor of the first enabled stage. The values for each ZoomingADC bloc are provided in **Table 37**:

Table 37. Capacitor values

PGA1 (with a gain of 10) and PGA2 (with a gain of 10) have each a minimum input impedance of 300 kOhm at $fs = 500$ kHz. PGA3 (with a gain of 10) have a minimum input impedance of 250 kOhm at $fs = 500$ kHz. Larger input impedance can be obtained by reducing the gain and/or by reducing the over-sampling frequency fs. Therefore, with a gain of 1 and a sampling frequency of 62.5 kHz, Zin > 10.2 MOhm for PGA1.

The input impedance on channels that are not selected is very high (>10MOhm).

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11.1.1 Switched Capacitor Principle

Basically, a switched capacitor is a way to emulate a resistor by using a capacitor. The capacitors are much easier to realize on CMOS technologies and they show a very good matching precision.

Figure 26. The Switched Capacitor Principle

A resistor is characterized by the current that flows through it (positive current leaves node V_1):

$$
I = \frac{V_1 - V_2}{R} \quad [A]
$$

Equation 2

One can verify that the mean current leaving node V_1 with a capacitor switched at frequency f is:

$$
\langle I \rangle = (V1 - V2) \cdot f \cdot C \quad [A]
$$

Equation 26

Therefore as a mean value, the switched capacitor $1/(f \times C)$ is equivalent to a resistor.

It is important to consider that this is only a mean value. If the current is not integrated (low impedance source), the impedance is infinite during the whole time but the transition. Figure 26. The Switched Capacitor Principle

Haracterized by the current that flows through it (positive current leaves node V_i):
 $I = \frac{V_1 - V_2}{R}$ [A]
 Equation 25
 Notify that the mean current leaving node V with **Equation 25**
 Equation 25
 Equation 26
 $\langle I \rangle = (V1 - V2) \cdot f \cdot C$ [A]
 Equation 26
 Condition 26
 Equation 26
 Condition 26
 Condition 26
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 Condition 26
 Condition 26
 Condit

What does it mean for the ZoomingADC?

If the fs clock is reduced, the mean impedance is increased. By dividing the fs clock by a factor 10, the impedance is increased by a factor 10.

One can reduce the capacitor that is switched by using an amplifier set to its minimal gain. In particular if PGA1 is used with gain 1, its mean impedance is 10x bigger than when it is used with gain 10.

Figure 27. The Switched Capacitor Principle

One can increase the effective impedance by increasing the electrical bandwidth of the sensor node so that the switching current is absorbed through the sensor before the switching period is over. Measuring the sensor node will

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show short voltage spikes at the frequency fs, but these will not influence the measurement. Whereas if the bandwidth of the node is lower, no spikes will arise, but a small offset can be generated by the integration of the charges generated by the switched capacitors, this corresponds to the mean impedance effect.

Notes:

- (1) One can increase the mean input impedance of the ZoomingADC by lowering the acquisition clock fs .
- (2) One can increase the mean input impedance of the ZoomingADC by decreasing the gain of the first enabled amplifier.
- (3) One can increase the effective input impedance of the ZoomingADC by having a source with a high electrical bandwidth (sensor electrical bandwidth much higher than fs).

11.2 Frequency Response

The incremental ADC is an over-sampled converter with two main blocks: an analog modulator and a low-pass digital filter. The main function of the digital filter is to remove the quantization noise introduced by the modulator. This filter determines the frequency response of the transfer function between the output of the ADC and the analog input VIN. Notice that the frequency axes are normalized to one elementary conversion period OSR / fs. The plots of **[Figure 28,](#page-49-2) [page 50](#page-49-2)** also show that the frequency response changes with the number of elementary conversions NELCONV performed. In particular, notches appear for NELCONV >= 2 These notches occur at:

$$
f_{NOTCH} = \frac{i \cdot f_s}{OSR \cdot N_{ELCONV}}
$$
 For $i = 1, 2, ... (N_{ELCONV} - 1)$

Equation 27

and are repeated every fs / OSR.

Information on the location of these notches is particularly useful when specific frequencies must be filtered out by the acquisition system. This chip has no dedicated 50/60 Hz rejection filtering but some rejection can be achieved by using **[Equation 27](#page-48-1)** and setting the appropriate values of OSR, fs and NELCONV.

Table 38. 50/60 Hz Line Rejection Examples

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Figure 28. Frequency Response. Normalized Magnitude vs. Frequency for Different NELCONV

11.3 Linearity

11.3.1 Integral Non-Linearity

The different PGA stages have been designed to find the best compromise between the noise performance, the integral non-linearity and the power consumption. To obtain this, the first stage has the best noise performance and the third stage the best linearity performance. For large input signals (small PGA gains, i.e. up to about 50), the noise added by the PGA is very small with respect to the input signal and the second and third stage of the PGA should be used to get the best linearity. For small input signals (large gains, i.e. above 50), the noise level in the PGA is important and the first stage of the PGA should be used.

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11.3.1.1 Gain 1

VBATT=5V ; VREF=VBATT; PGAs disabled; OSR=1024 ; Nelconv=8 ; fs=250kHz; Resolution=16bits.

11.3.1.2 Gain 10

VBATT=5V ; VREF=VBATT; ADC and PGA3 enabled ; GD3=10; OSR=1024 ; Nelconv=8 ; fs=250kHz; Resolution=16bits.

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11.3.1.3 Gain 100

VBATT=5V ; VREF=VBATT; ADC, PGA2 and PGA3 enabled ; GD2=10; GD3=10; OSR=1024 ; Nelconv=8 ; fs=250kHz; Resolution=16bits.

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11.3.1.4 Gain 1000

VBATT=5V ; VREF=VBATT; ADC, PGA3, PGA2, PGA1 enabled; GD1=10, GD2=10, GD3=10; OSR=1024 ; NELCONV=8 ; fs=250KHz; Resolution=16bits.

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11.3.2 Differential Non-Linearity

The differential non-linearity is generated by the ADC. The PGA does not add differential non-linearity. **[Figure 45](#page-53-2)** shows the differential non-linearity.

Figure 45. Differential Non-Linearity of the ADC Converter

11.4 Noise

Ideally, a constant input voltage V_{IN} should result in a constant output code. However, because of circuit noise, the output code may vary for a fixed input voltage. Thus, a statistical analysis on the output code of 1200 conversions for a constant input voltage was performed to derive the equivalent noise levels of PGA1, PGA2, and PGA3.

The extracted rms output noise of PGA1, 2, and 3 are given in **Table 39, page 56**: standard output deviation and output rms noise voltage.

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Figure 46. Simple Noise Model for PGAs and ADC

VN1, VN2, and VN3 are the output rms noise figures of **Table 39**, GD1, GD2, and GD3 are the PGA gains of stages 1 to 3 respectively. VREFN, WB is the wide band noise on the reference voltage.

The simple noise model of **Figure 46** is used to estimate the equivalent input referred rms noise V_{N/N} of the acquisition chain in the model of **Figure 48, page 56**. This is given by the relationship:

ofisets:
\n**Figure 46. Simple Noise Model for PGAs and ADC**
\n*VN1, VN2*, and *VN3* are the output rms noise figures of **Table 39**, *GD1*, *GD2*, and *GD3* are the *PGA* gains of stages 1 to 3 respectively. *VREFN, WB* is the wide band noise on the reference voltage.
\nThe simple noise model of **Figure 48, page 56**. This is given by the relationship:
\nchain in the model of **Figure 48, page 56**. This is given by the relationship:
\n
$$
V_{N,N^2} = \frac{\left(\frac{V_{N1}}{GD_1}\right)^2 + \left(\frac{V_{N2}}{GD_1 \cdot GD_2}\right)^2 + \left(\frac{V_{N3}}{GD_{TOT}}\right)^2 + \left(\frac{V_{KEYN, WB}}{GD_{TOT}}\right)^2 + \left(\frac{V_{KEYN, WB}}{GD_{TOT}}\right)^2 + \left(\frac{1}{2} \cdot \frac{V_{KEYN, WB}}{GD_{TOT}}\right)^2}{(OSR \cdot N_{ELCONV})} \left[V^2rms\right]
$$

Equation 28

On the numerator of **Equation 28** :

- 1 the first parenthesis is the PGA1 gain amplifier contribution to noise
- 2 the second parenthesis is the PGA2 gain amplifier contribution to noise
- 3 the third parenthesis is the PGA3 gain amplifier contribution to noise
- 4 the fourth parenthesis is PGA2 and PGA3 offset amplifiers contributions to noise
- 5 the last parenthesis is the contribution of the noise on the references of the ADC

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As shown in **[Equation 28](#page-54-0)**, noise can be reduced by increasing OSR and NELCONV (increases the ADC averaging effect, but reduces noise).

Table 39. PGA Noise Measurement (n = 16bits, OSR = 512, NELCONV = 2, VREF = 5V)

[Figure 47](#page-55-2) shows the distribution for the ADC alone (PGA1, 2, and 3 bypassed). Quantization noise is dominant in this case, and, thus, the ADC thermal noise is below 16 bits.

Figure 47. ADC Noise (PGA1, 2 & 3 Bypassed, OSR = 512, NELCONV = 2)

Figure 48. Total Input Referred Noise

As an example, consider the system where: $GD2 = 10$ ($GD1 = 1$; PGA3 bypassed), $OSR = 512$, NELCONV = 2, VREF = 5 V. In this case, the noise contribution *VN1* of PGA1 is dominant over that of PGA2. Using **[Equation 28, page 55](#page-54-0)**, we get: VN,IN = 6.4 μV (rms) at the input of the acquisition chain, or, equivalently, 0.85 LSB at the output of the ADC. Considering 0.2 V (rms) maximum signal amplitude, the signal-to-noise ratio is 90dB.

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11.5 Gain Error and Offset Error

Gain error is defined as the amount of deviation between the ideal transfer function (theoretical **[Equation 19, page](#page-32-6) [33](#page-32-6)**) and the measured transfer function (with the offset error removed).

The actual gain of the different stages can vary depending on the fabrication tolerances of the different elements. Although these tolerances are specified to a maximum of $\pm 3\%$, they will be most of the time around $\pm 0.5\%$. Moreover, the tolerances between the different stages are not correlated and the probability to get the maximal error in the same direction in all stages is very low. Finally, these gain errors can be calibrated by the software at the same time with the gain errors of the sensor for instance.

[Figure 49](#page-56-1) shows gain error drift vs. temperature for different PGA gains. The curves are expressed in % of Full-Scale Range (FSR) normalized to 25°C.

Offset error is defined as the output code error for a zero volt input (ideally, output code $= 0$). The offset of the ADC and the PGA1 stage are completely suppressed if NELCONV > 1.

The measured offset drift vs. temperature curves for different PGA gains are depicted in **Figure 50**. The output offset error, expressed in LSB for 16-bit setting, is normalized to 25°C. Notice that if the ADC is used alone, the output offset error is below +/-1 LSB and has no drift.

Figure 49. Gain Error vs. Temperature for Different Gains Figure 50. Offset Error vs. Temperature for Different Gains

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11.6 Power Consumption

[Figure 51](#page-57-1) plots the variation of current consumption with supply voltage VBATT, as well as the distribution between the 3 PGA stages and the ADC (see **[Table 40, page 60](#page-59-0)**). The Charge Pump is forced ON for VBATT < 4.2V and forced OFF for V BATT $> 4.2V$.

Figure 51. Current Consumption vs. Supply Voltage and PGAs

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As shown in **[Figure 52](#page-58-0)**, if lower sampling frequency is used, the current consumption can be lowered by reducing the bias currents of the PGAs and the ADC with registers IbAmpPga and IbAmpAdc. (In **[Figure 52](#page-58-0)**, IbAmpPga/Adc = '11', '10', '00' for fs = 500, 250, 62.5 kHz respectively. The Charge Pump is forced ON for VBATT < 4.2V and forced OFF for VBATT > 4.2V.

Figure 52. Current Consumption vs Temperature and ADC Sampling Frequency

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Current consumption vs. temperature is depicted in **[Figure 53](#page-59-1)**, showing the increase between -40 and +125°C.

Figure 53. Current Consumption vs Temperature and Supply Voltage

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FAMILY OVERVIEW

This chapter gives an overview of similar devices based on the ZoomingADC but with different features or packages. Each part is described in it's own datasheet.

12 Comparizon table

Table 41. Family comparizon table

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13 Comparizon by package pinout

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MECHANICAL

14 PCB Layout Considerations

PCB layout considerations to be taken when using the SX8725C are relatively simple to get the highest performances out of the ZoomingADC. The most important to achieve good performances out the ZoomingADC is to have a good voltage reference. The SX8725C has already an internal reference that is good enough to get the best performances with a minimal amount of external components, but, in case an external reference is needed this one must be as clean as possible in order to get the desired performance. Separating the digital from the analog lines will be also a good choice to reduce the noise induced by the digital lines. It is also advised to have separated ground planes for digital and analog signals with the shortest return path, as well as making the power supply lines as wider as possible and to have good decoupling capacitors. ence. The SX8725C has already an internal reference that is good enough to get the best and a
nal amount of external components, but, in case an external reference is needed this one
order to get the desired performance. S

15 How to Evaluate

For evaluation purposes SX8724CEVK evaluation kit can be ordered. This kit connects to any PC using a USB port. The "SX87xx Evaluation Tools" software gives the user the ability to control the SX8725C registers as well as getting the raw data from the ZoomingADC and displaying it on the "Graphical User interface". For more information please look at SEMTECH web site (**http://www.semtech.com**). **New York Control** and Section Control the SX8725C regist
uying it on the "Graphical User interface". For more is
ech.com).

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16 Package Outline Drawing: 4x4MLPD-W12-EP1

2. COPLANARITY APPLIES TO THE EXPOSED PAD AS WELL AS TERMINALS 1. CONTROLLING DIMENSIONS ARE IN MILLIMETERS (ANGLES IN DEGREES).

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NOTES:

- CONTROLLING DIMENSIONS ARE IN MILLIMETERS (ANGLES IN DEGREES). 1.
- COPLANARITY APPLIES TO THE EXPOSED PAD AS WELL AS THE TERMINALS. 2.

Figure 54. Package Outline Drawing

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17 Land Pattern Drawing: 4x4MLPD-W12-EP1

NOTES:

- 1. CONTROLLING DIMENSIONS ARE IN MILLIMETERS (ANGLES IN DEGREES).
- THIS LAND PATTERN IS FOR REFERENCE PURPOSES ONLY. 2. CONSULT YOUR MANUFACTURING GROUP TO ENSURE YOUR COMPANY'S MANUFACTURING GUIDELINES ARE MET.
- THERMAL VIAS IN THE LAND PATTERN OF THE EXPOSED PAD 3. SHALL BE CONNECTED TO A SYSTEM GROUND PLANE. FUNCTIONAL PERFORMANCE OF THE DEVICE. FAILURE TO DO SO MAY COMPROMISE THE THERMAL AND/OR **New SEARCH CONSTANT CONSTANT OF THE CONSTANT OF THE DEVICE SEARCH CONFIRMAL AND PATTERN OF THE EXPOSED PADEMAND COMPROMISE THE THERMAL AND/OR**
AND PATTERN OF THE EXPOSED PADEMAND COMPROMISE THE THERMAL AND/OR
TO A SYSTEM

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18 Tape and Reel Specification

MLP/QFN (0.70mm - 1.00mm package thickness)

- Single Sprocket holes
- Tolerances for Ao & Bo are +/-0.20mm
- \blacksquare Tolerances for Ko is $+/$ -0.10mm
- Tolerance for Pocket Pitch is +/-0.10mm
- \blacksquare Tolerance for Tape width is $+/-0.30$ mm
- Trailer and Leader Length are minimum required length
- **Package Orientation and Feed Direction**

Table 42. Tape and reel specifications

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